

19.1

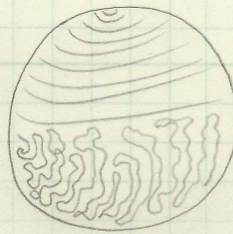
Bicycle crank

rupture

Fatigue
crack
propagation

initiation

The fracture surface resembles the typical fatigue fracture surface due to cyclic loading
(initiation → Fatigue crack propagating → rupture)
Clam shell marks



typical fatigue

fracture surface

- (b) see figure above on the left
- (c) rupture part
- (d) at the bottom of the thread
- (e) moderate

20.1

$$\dot{\epsilon} = A \sigma^5 e^{-Q/RT}$$

$$\ln \dot{\epsilon} = \ln(A \sigma^5 e^{-Q/RT})$$

$$\ln \dot{\epsilon} = \ln(A \sigma^5) + \ln(e^{-Q/RT})$$

$$\ln \dot{\epsilon} = \ln(A \sigma^5) - \frac{Q}{RT} \ln e$$

$$\ln \dot{\epsilon} = \underbrace{\ln(A \sigma^5)}_{\text{Intercept } y_0} + \underbrace{\left(\frac{-Q}{R}\right) \frac{1}{T}}_{\text{slope } m}$$

$$\sigma = \frac{Pr}{t} = \frac{(6 \text{ MNm}^{-2})(\frac{40 \times 10^{-3}}{2})}{2 \times 10^{-3}}$$

$$\sigma = 60 \text{ MNm}^{-2}$$

Plot: $\ln \dot{\epsilon}$ vs. $1/T$

look at data sheet & graph

$$\ln \dot{\epsilon} = \underbrace{16.991}_{y_0} - \underbrace{29597}_{\text{slope}} \left(\frac{1}{T} \right)$$

$$\ln(A \sigma^5) = 16.991 \Rightarrow A \sigma^5 = e^{16.991} \Rightarrow A = 7.5 \times 10^{-35}$$

$$\frac{Q}{R} = 29597$$

$$\dot{\epsilon} = A \sigma^5 e^{-Q/RT}$$

$$\begin{aligned} \text{@ } 510^\circ\text{C} \quad \dot{\epsilon} &= 7.5 \times 10^{-35} (200 \times 10^6)^5 e^{-29597 \left(\frac{1}{510+273} \right)} \\ &= 2.23 \times 10^{-12} \text{ s}^{-1} \end{aligned}$$

$$\epsilon = \dot{\epsilon} \times t$$

$$t = 9 \text{ years} = 2.8 \times 10^8 \text{ s}$$

$$\epsilon = 2.23 \times 10^{-12} \times 2.8 \times 10^8$$

$$\epsilon = 0.00057 < 0.01 \Rightarrow \text{design safe.}$$

20.2

$$\dot{\epsilon} = A \sigma^5 e^{-Q/RT}$$

$$\sigma_1 = 25 \text{ MN m}^{-2}$$

$$T_1 = 620 + 273 = 893 \text{ K}$$

$$\dot{\epsilon}_1 = 3.1 \times 10^{-12} \text{ s}^{-1}$$

$$\sigma_2 = 30 \text{ MN m}^{-2}$$

$$T_2 = 650 + 273 = 923 \text{ K}$$

$$Q = 160 \times 10^3 \text{ J/mol}$$

$$\dot{\epsilon}_1 = A \sigma^5 e^{-Q/RT_1}$$

$$A = \frac{\dot{\epsilon}_1}{\sigma^5 e^{-Q/RT_1}} = \frac{3.1 \times 10^{-12}}{(25 \times 10^6)^5 e^{-160 \times 10^3 / (8.31 \times 893)}}$$

$$A = 7.34 \times 10^{-40}$$

$$\dot{\epsilon}_2 = (7.34 \times 10^{-40}) (30 \times 10^6)^5 e^{-\frac{160 \times 10^3}{8.31 \times (650 + 273)}}$$

$$\dot{\epsilon}_2 = 1.55 \times 10^{-11} \text{ s}^{-1}$$

$$\begin{aligned} \dot{\epsilon}_{\text{ave}} &= 0.30 [1.55 \times 10^{-11}] + 0.70 [3.1 \times 10^{-12}] \\ &= 6.8 \times 10^{-12} \text{ s}^{-1} \end{aligned}$$

20.6

Although steel will not melt, creep might be a problem when the temp. is too high. (above melting temp.)