

# Concentrated Solar Thermal Power Technology

Prof. G.R. Tynan

MANY SLIDES ADOPTED FROM  
A TALK AT 2005 AAAS MEETING

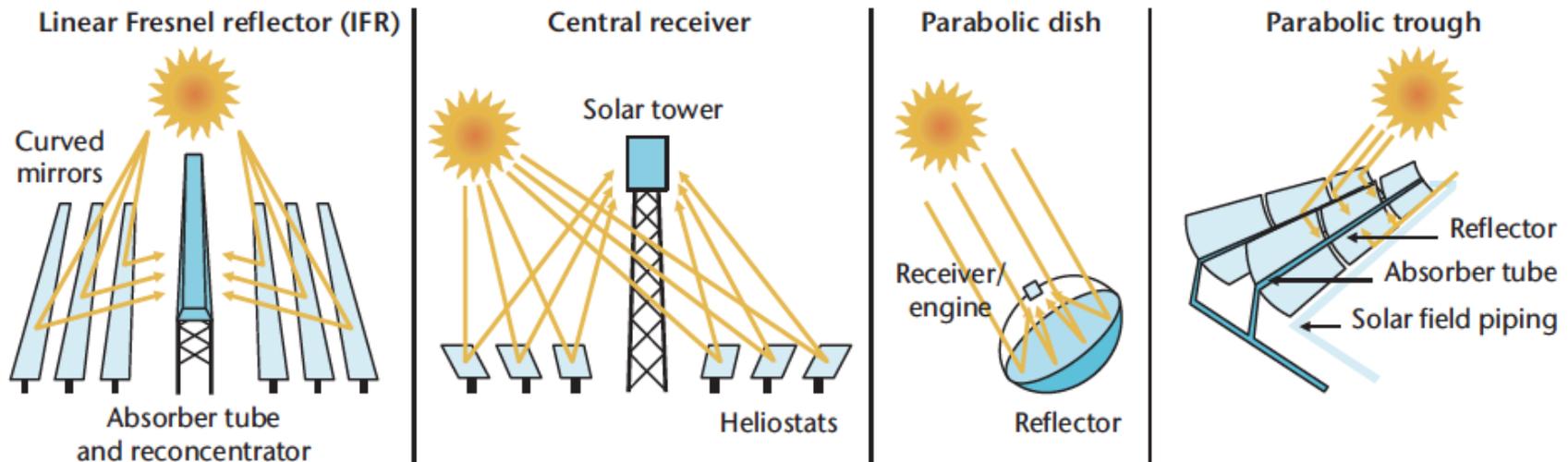
BY  
E. BOES, NREL

And

Professor Carlos Coimbra, UCSD-MAE & CER

# Three Main Solar Thermal Electric System Architectures

Figure 3: Main CSP technologies



**KEY POINT:** Most current CSP plants are based on trough technology, but tower technology is increasing and linear Fresnel installations emerging.

# Three Main Solar Thermal Electric System Architectures

**Trough Technology (Bulk Power)**

(a)



**Dish/Engine Technology  
(Distributed Power)**

(b)



(c)

**Power Tower  
Technology  
(Bulk Power)**



# Utility Scale Central Plants

## California Valley Solar Ranch, 250 MW Single-Axis Tracking



# Concentrating Parabolic Trough Technology

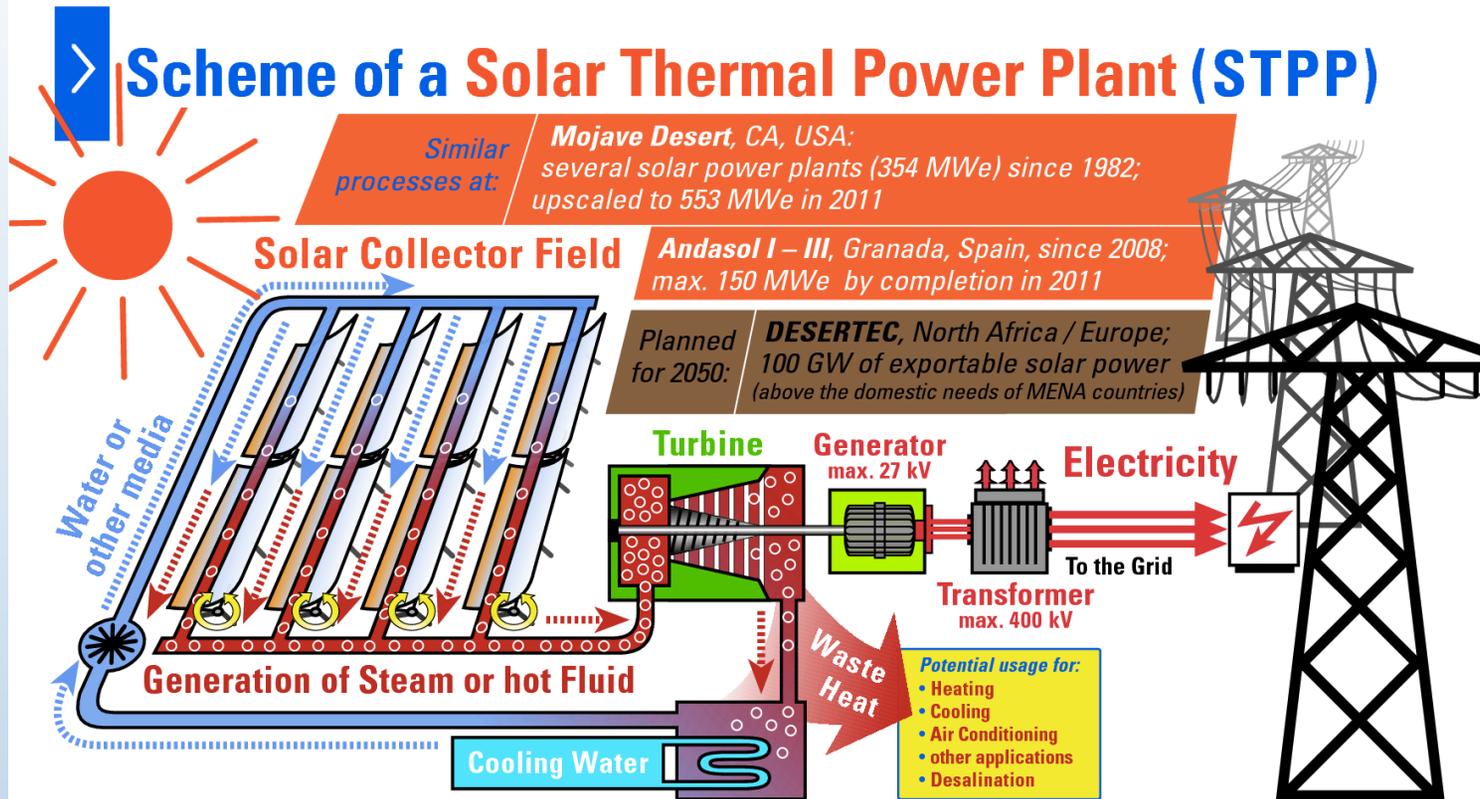


# Helioestat Array & Power Tower



Ivanpah Solar Electric Generation System,  
[www.brightsourceenergy.com](http://www.brightsourceenergy.com)

# System schematic



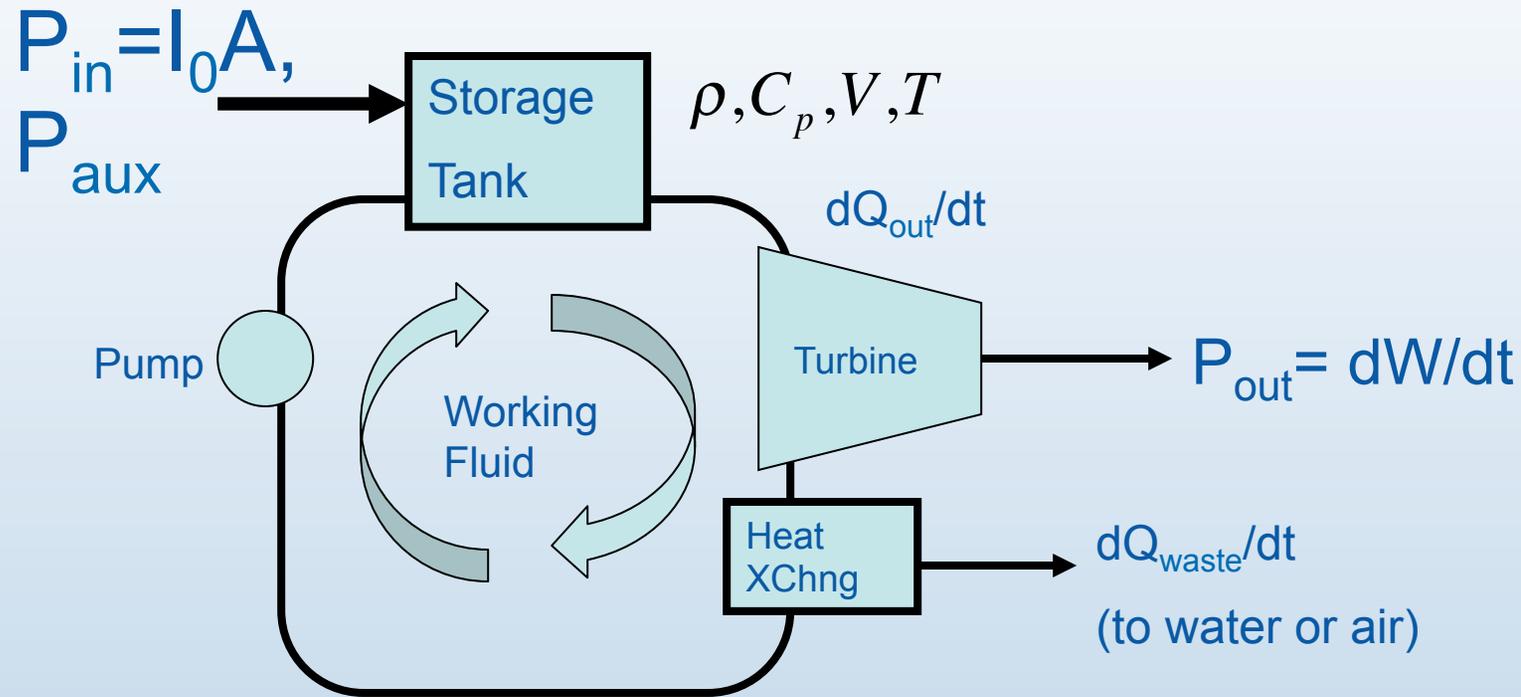
Go to where the market is! [www.fair-pr.com](http://www.fair-pr.com) I M P L E M E N T I N G N E W I D E A S

Source: [www.shp-europe.com](http://www.shp-europe.com), own research

EVERS

First released: August 2007; latest update: July 2009

# Schematic of Solar Thermal Plant w/ Thermal Storage



Energy Balance at Storage Tank Gives

$$\rho C_p V \frac{\partial T}{\partial t} = P_{in} + P_{aux} - \frac{dQ_{out}}{dt}$$

Energy Balance at Turbine Gives

$$\frac{dQ_{out}}{dt} = \frac{dW}{dt} + \frac{dQ_{waste}}{dt}$$

# Analysis of Solar Thermal Heat Balance- Steady-state Day Operation

Add two together & use def'n of  $P_{out}$

$$\frac{dQ_{out}}{dt} = P_{out} + \frac{dQ_{waste}}{dt}; \quad P_{out} = dW / dt; \quad W = \eta_{th} Q_{out}$$

thus

$$\rho C_p V \frac{\partial T}{\partial t} = P_{in} + P_{aux} - \frac{1}{\eta_{th}} P_{out}$$

With Solar Input Only Then Have

$$\rho C_p V \frac{\partial T}{\partial t} = P_{in} + \cancel{P_{aux}} - \frac{1}{\eta_{th}} \frac{dW}{dt} \Rightarrow P_{in} = \frac{1}{\eta_{th}} \frac{dW}{dt} \text{ in } S.S.$$

↑  
Steady-state!

# Analysis of Solar Thermal Heat Balance- Transient Night Operation

At Night Have No Power Input

$$P_{in} = 0 \text{ \& } P_{aux} = 0$$

Transient Heat Balance Gives

$$\rho C_p V \frac{\partial T}{\partial t} = - \frac{1}{\eta_{th}} \frac{dW}{dt}$$

If Have Exponential Like Decay,  $T \sim e^{-t/\tau}$

$$\rho C_p V \left( -\frac{T}{\tau} \right) = - \frac{1}{\eta_{th}} \frac{dW}{dt} \Rightarrow \tau = \frac{\rho C_p V T \eta_{th}}{dW / dt}$$

# Transient Night Operation of Solar Thermal Plant

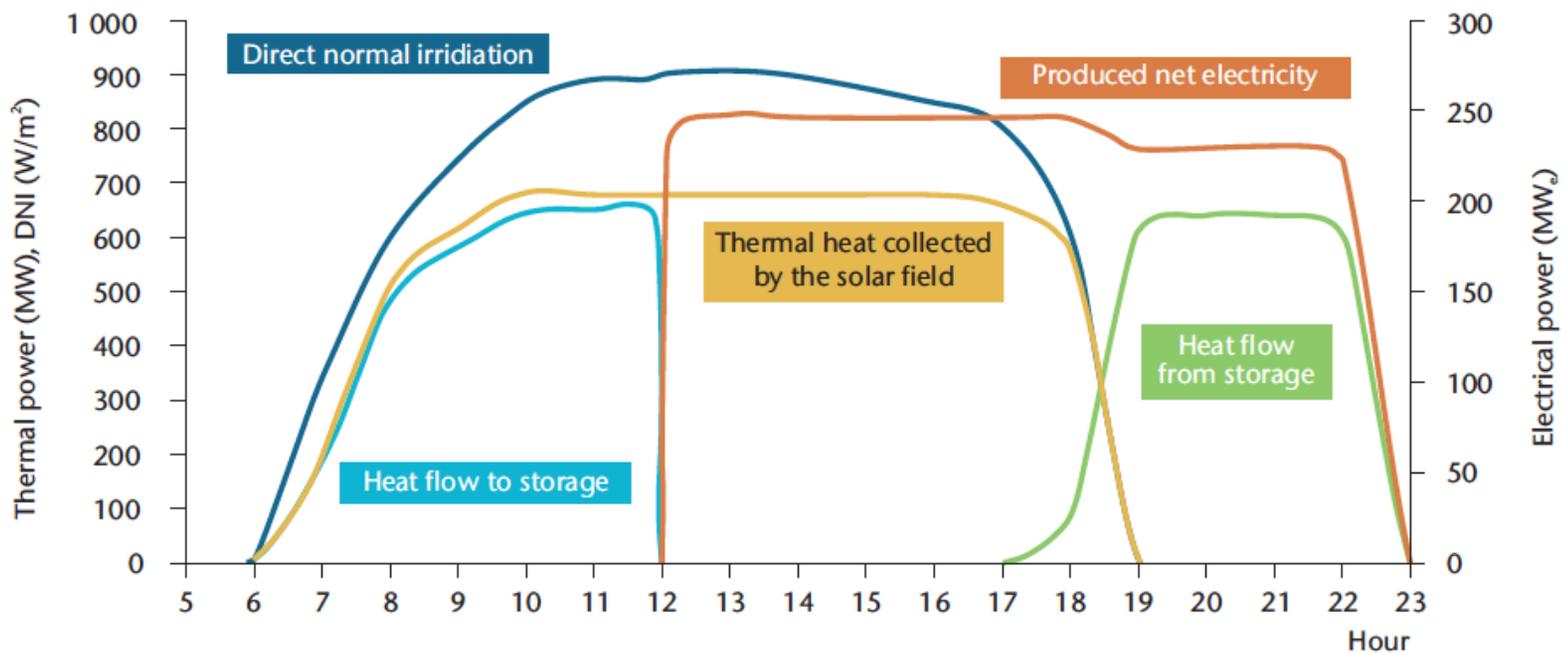
Key Conclusion: Can make Power at Night  
IF  $V$  large enough and/or  $dW/dt$  Small Enough

$$\tau = \frac{\rho C_p VT \eta_{th}}{dW / dt} > 24 \text{hours}$$

Adding  $P_{aux}$  (e.g. from Gas Fired Heat Input) Allows Additional Backup Capability

# Thermal Storage Enables Dispatchability; Load Shifting

Figure 4: Use of storage for shifting production to cover evening peaks



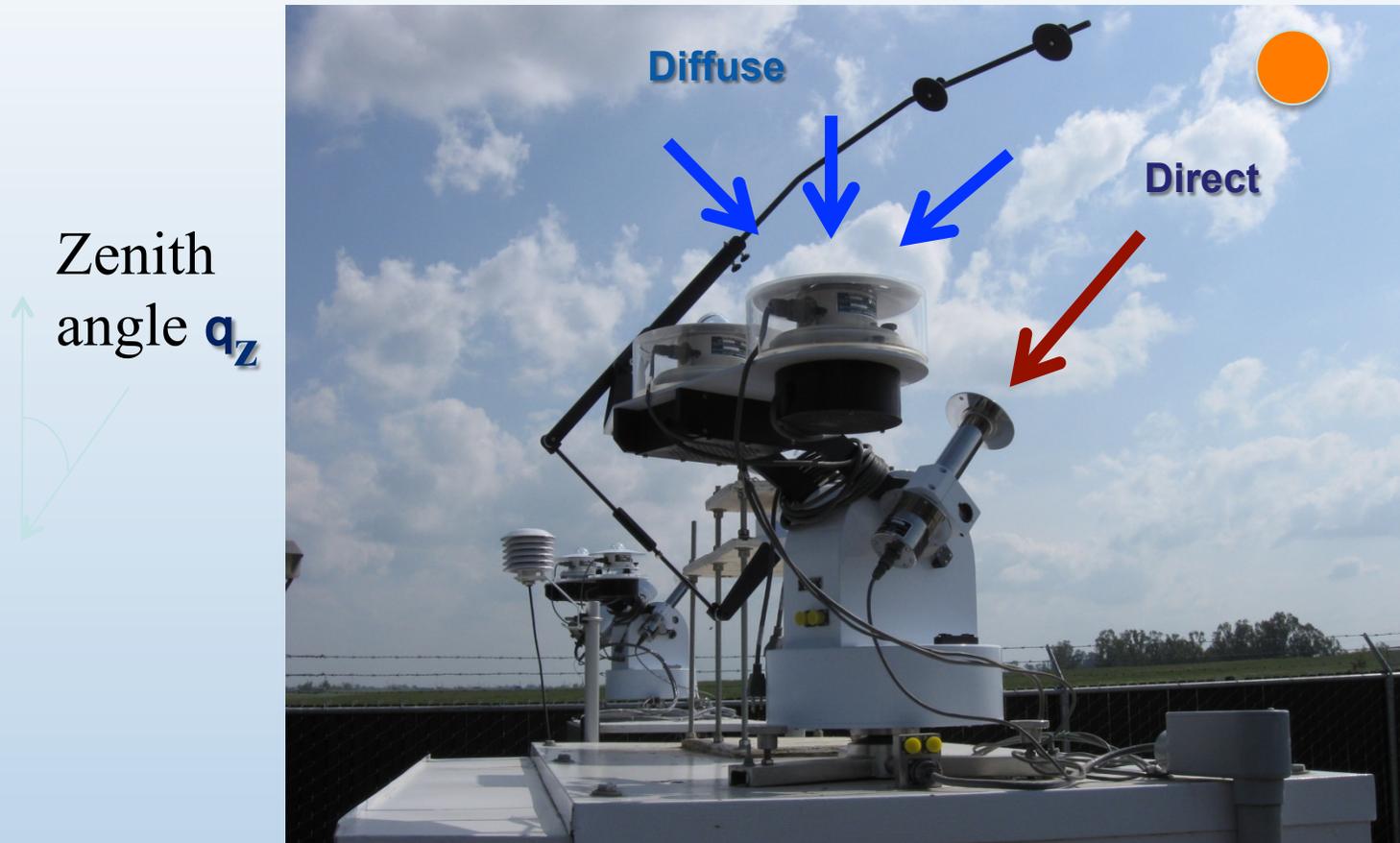
Notes: the graph shows on left scale the DNIR and the flows of thermal exchanges between solar field, storage and power block, and on the right scale electricity generation of a 250-MW (net) CSP plant with storage. Courtesy of ACS Cobra.

**KEY POINT:** Thermal storage uncouples electricity generation from solar energy collection.

# Three types of solar irradiation

- **Direct normal incidence (DNI):**  
intensity of unscattered light coming directly from sun, normal to a surface
- **Diffusive horizontal incidence (DHI):**  
intensity of scattered irradiation incident on a horizontal surface
- **Global horizontal irradiance (GHI):**  
DHI + direct irradiance to a horizontal surface

# Difference between direct normal irradiance (DNI) and global horizontal irradiance (GHI)

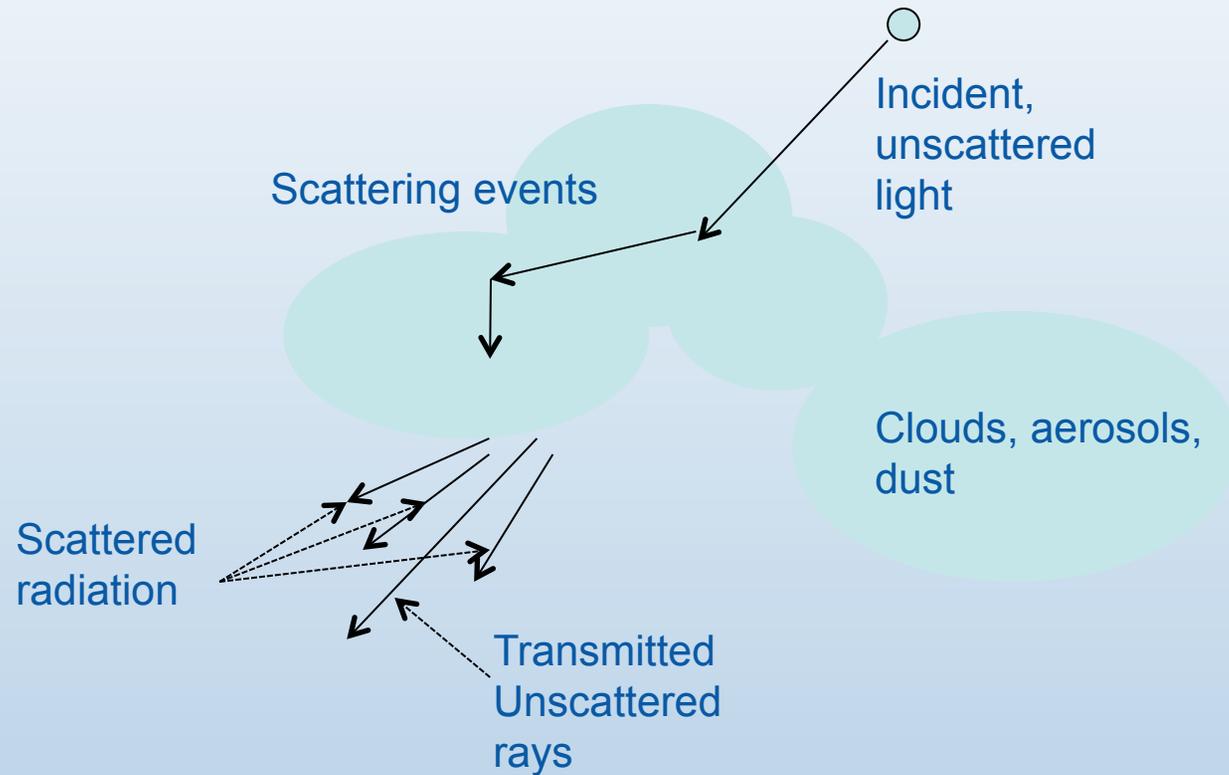


$$\text{GHI} \sim \text{Direct} \cdot \cos q_z + \text{Diffuse}$$

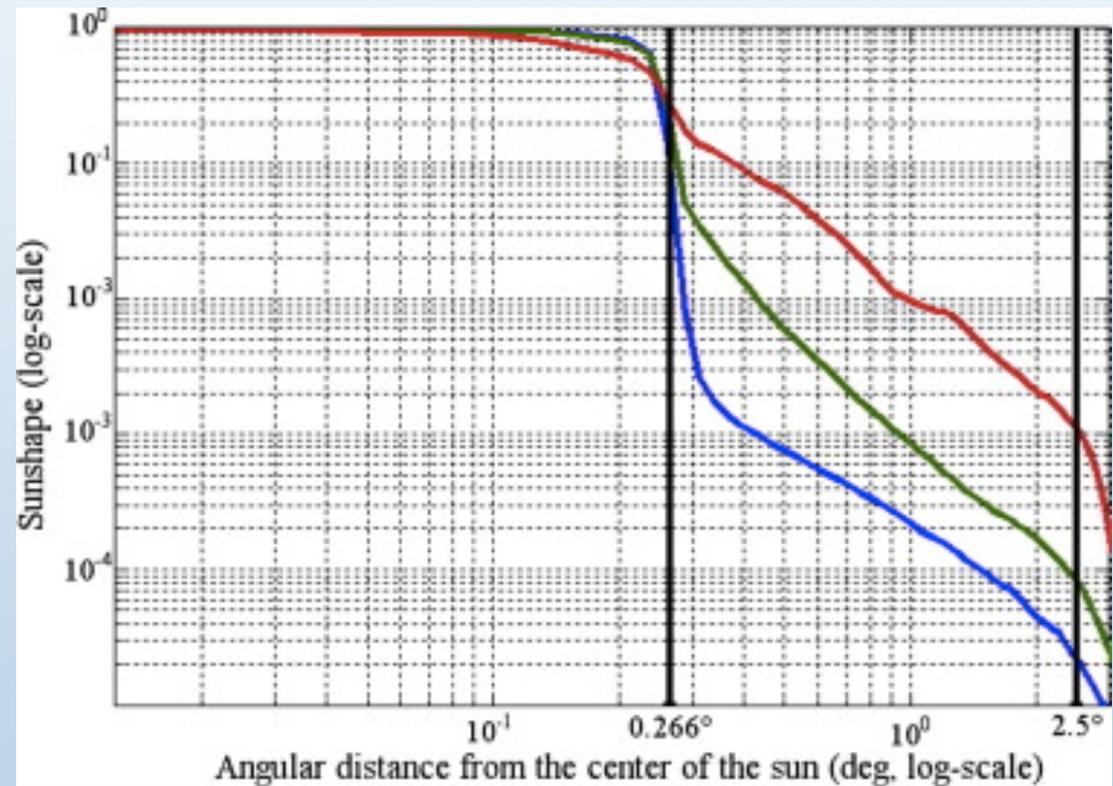
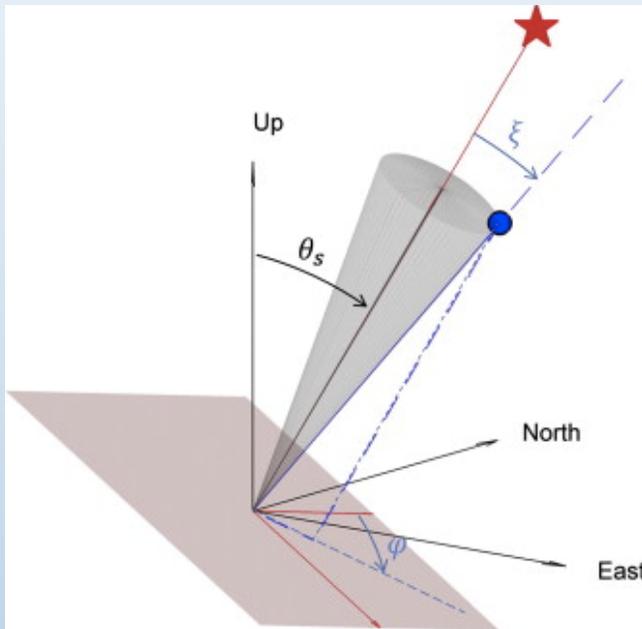
# Concentrated Solar Power (CSP)

- **Requires direct-beam solar radiation (more in a moment)**
- Uses familiar components & technologies – glass, steel, gears, heat exchangers, turbines
- Can provide dispatchable power IF:
  - Thermal storage is incorporated, or
  - Hybridized with natural gas

# Clouds, Dust & Aerosols Act to Scatter Solar Radiation → Reduced DNI



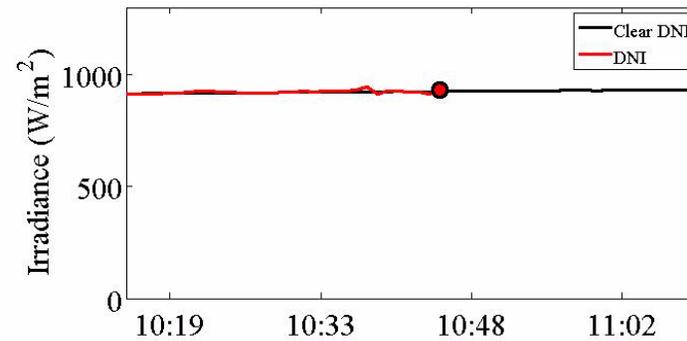
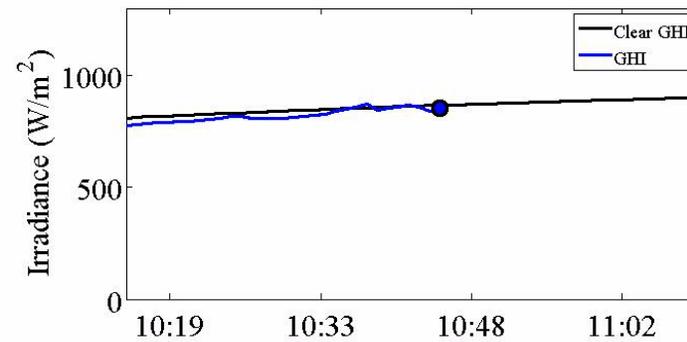
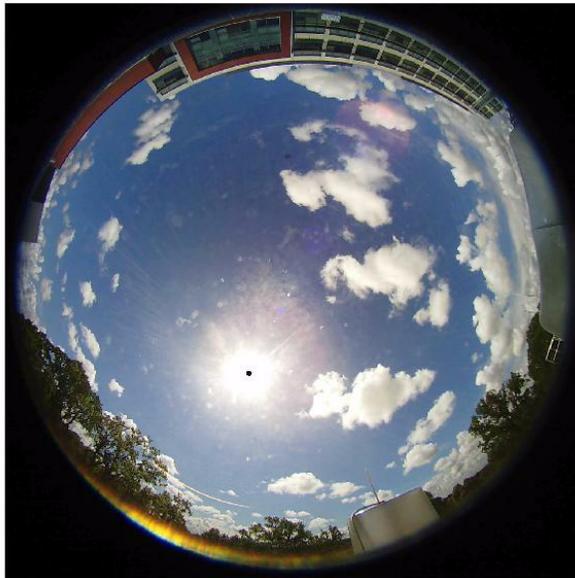
# Clouds, Dust & Aerosols Act to Scatter Solar Radiation → Reduced DNI



# Effect of clouds on solar irradiance at the ground level

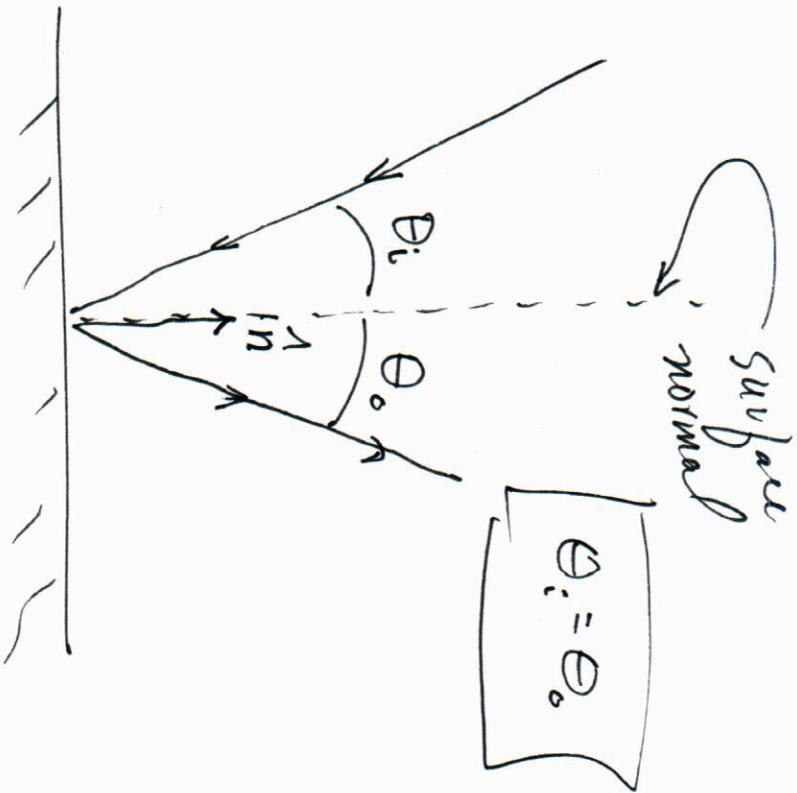


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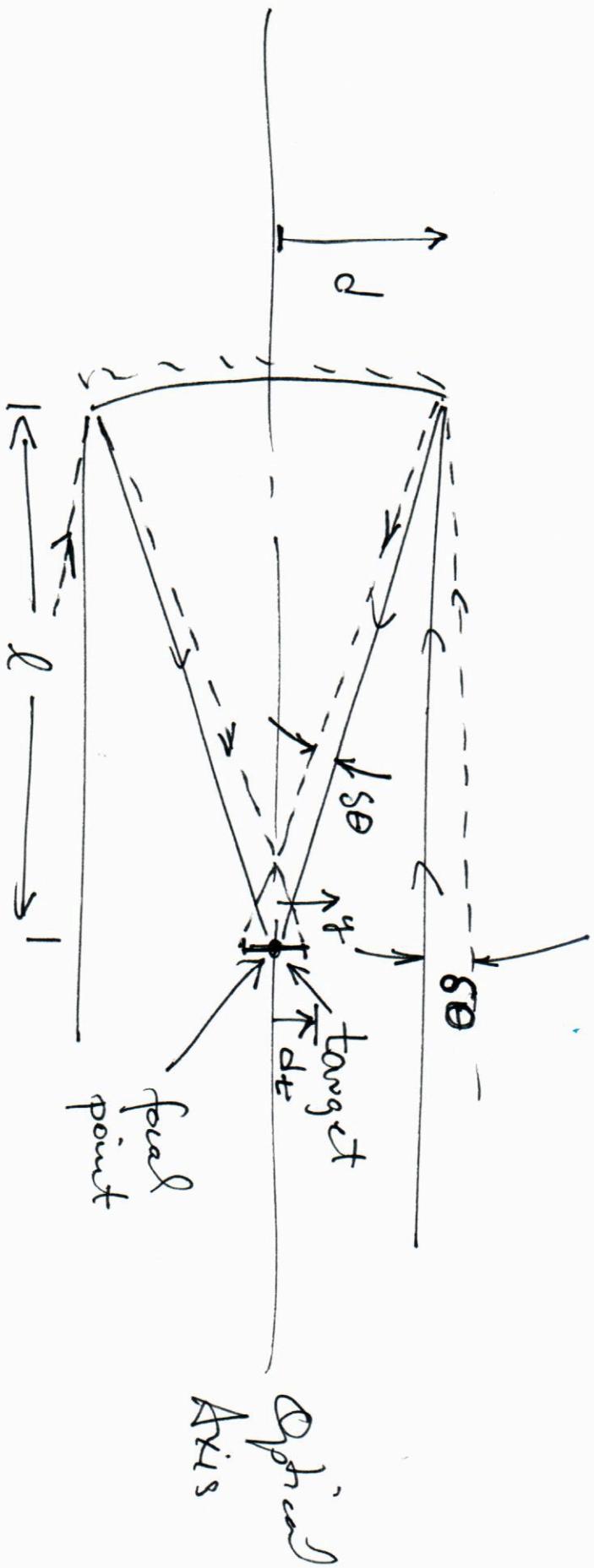


**Review Specular Reflection,  
Focusing Optics Acceptance  
Angle and  
Radiation Scattering**

Remember Basic Concept of Specular Reflection



Consider focusing optics based system:



$d \sim$  radius of primary optical element

$l \sim$  focal length

$d_t \sim$  radius of target

$\delta\theta \sim$  deviation of rays from parallel to optical axis

Define the so-called  $f$ -number of the optics as

$$f \equiv \frac{f}{\sigma} \sim \frac{\text{ratio of focal length}}{\text{optical element size}}$$

from geometry, the rays defined by the dashed line are displaced away from the focal point. This distance is given by

$$S_y = l \tan \theta.$$

for small  $\theta \ll 1$ ,

$$S_y \approx l \theta$$

Now... if  $S_y > d_t$  then the collected light misses the target! Thus we require

$$d_t \leq S_y$$

or

$$d_t \leq R S_\theta$$

Solving for maximum allowable  $S_\theta$ :

$$S_\theta \leq \frac{d_t}{R}$$



An important parameter is the concentration ratio,  $C$

$$C \equiv \frac{d}{d_t} \gg 1$$

← usually

~~Apply~~ Solving for  $d_t$  gives  $d_t = \frac{d}{C}$

and so we can write

$$S\theta \leq \frac{1}{C} \frac{d}{\lambda}$$

or

$$S\theta \leq \frac{1}{C} \frac{1}{f}$$

Considers two main types of system geometry

Trough:  $d \sim \text{few m}$   $\lambda \sim d \rightarrow f \sim 1$

$$C \sim 10^2 \text{ or } 30 \dots \rightarrow S\theta \leq \frac{1}{10^2} \frac{1}{1} \sim 10^{-2} \text{ radian}$$

Power Tower

$$d \sim 100 - 1000 \text{ m}$$

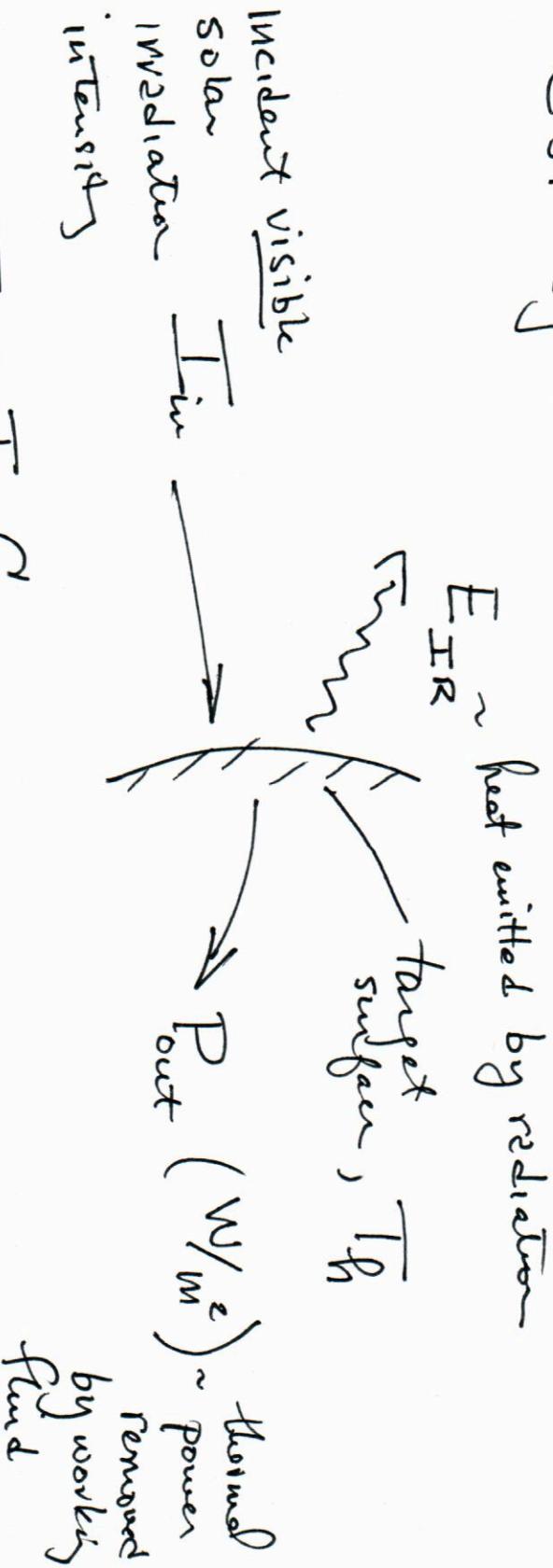
$$\lambda \sim d \sim 100 - 1000 \text{ m}$$

$$\lambda \sim f \sim 1 \quad C \sim 10^2 - 10^3$$

$$S\theta \leq \frac{1}{10^2} - \frac{1}{10^3} \sim 10^{-3} \rightarrow 10^{-2} \text{ radian}$$

What value of  $C$  do we want?

Consider power balance at target of the CSP system



power balance gives:

$$I_{in} = E_{IR} + P_{out} \quad ; \quad w/ \quad E_{IR} = \sigma T_R^4$$

$$I_{in} = I_0 C$$

$$I_0 C = \sigma T_R^4 + P_{out}$$

we wish to make  $T_R$  as high as possible  
(with materials limits) to maximize  $\eta_{th}$   
Solve for  $T_R$

$$T_R = \sqrt[4]{\frac{1}{\sigma} (I_0 C - P_{out})}$$

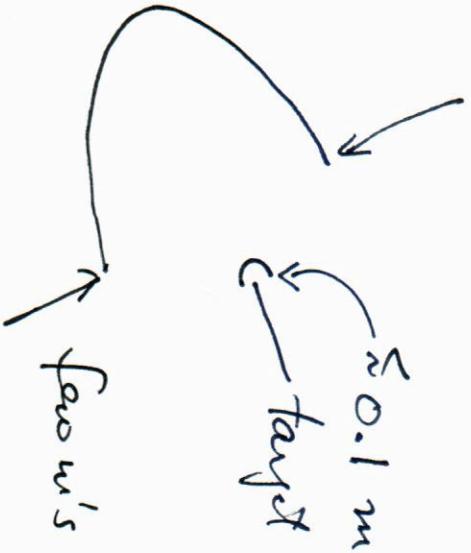
for a given  $P_{out}$ ,  $I_0 \Rightarrow$  Maximizing  $C$ !

look at typ systems:

Trough System

$$C \sim \frac{3-5 \text{ m}}{0.05-0.1 \text{ m}}$$

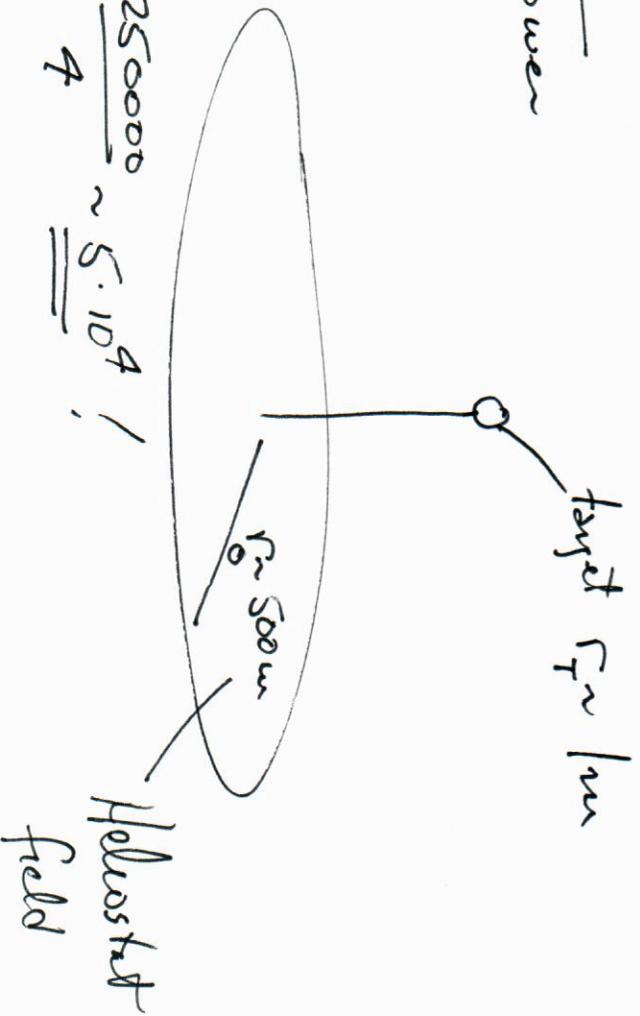
$$\sim \underline{\underline{30-100}}$$



Power Tower

$$C \sim \frac{4\pi r_0^2}{4\pi r_T^2}$$

$$\sim \frac{500^2}{4 \cdot 12^2} \approx \frac{250000}{4} \sim \underline{\underline{5 \cdot 10^4}}$$



Estimate  $T_a$ :

$$T \sim 6 \times 10^{-8} \text{ W/m}^2 \text{ K}^4$$

thermal power in one tower at launch  $\sim 300 \text{ MW}$

$$P = 300 \text{ MW} / A_t \sim 3 \cdot 10^8 / (4 \cdot \pi \cdot 2^2) \sim 3 \cdot 10^7 \text{ W/m}^2$$

Helio-stead area  $A \sim \pi r_0^2 \sim 3 \cdot 5 \cdot 10^4 \sim 75 \cdot 10^4 \sim 10^6 \text{ m}^2$

$$I_0 \sim 400 \text{ W/m}^2$$

$$G \sim 5 \cdot 10^4$$

$$\therefore T_a = \sqrt[4]{\frac{1}{6 \cdot 10^{-8}} (4 \cdot 10^2 \cdot 5 \cdot 10^4 - 3 \cdot 10^7)}$$

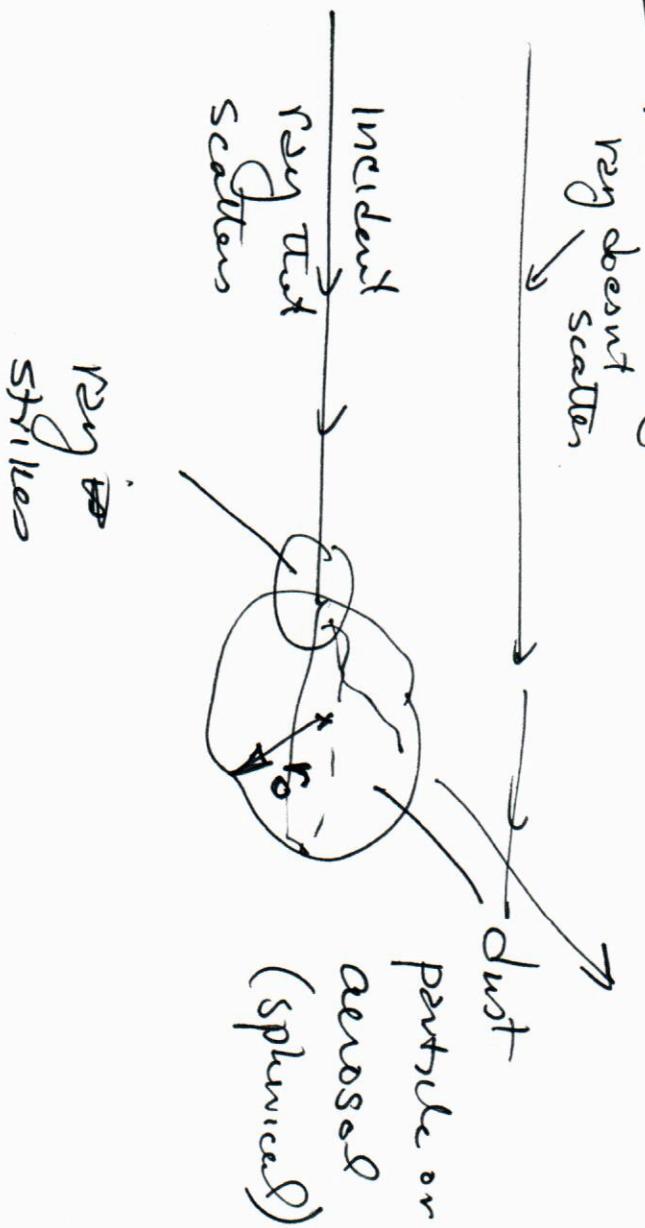
$$T_a = \sqrt[4]{\frac{1}{6 \cdot 10^{-8}} (4 \cdot 10^2 \cdot 5 \cdot 10^4 - 3 \cdot 10^7)}$$

$$= \sqrt[4]{\frac{10^{15}}{6 \cdot 10^{-8}} \approx 10^{14}}$$

$$= \sqrt[4]{10^7} \approx \underline{\underline{3000 \text{ K}}}$$

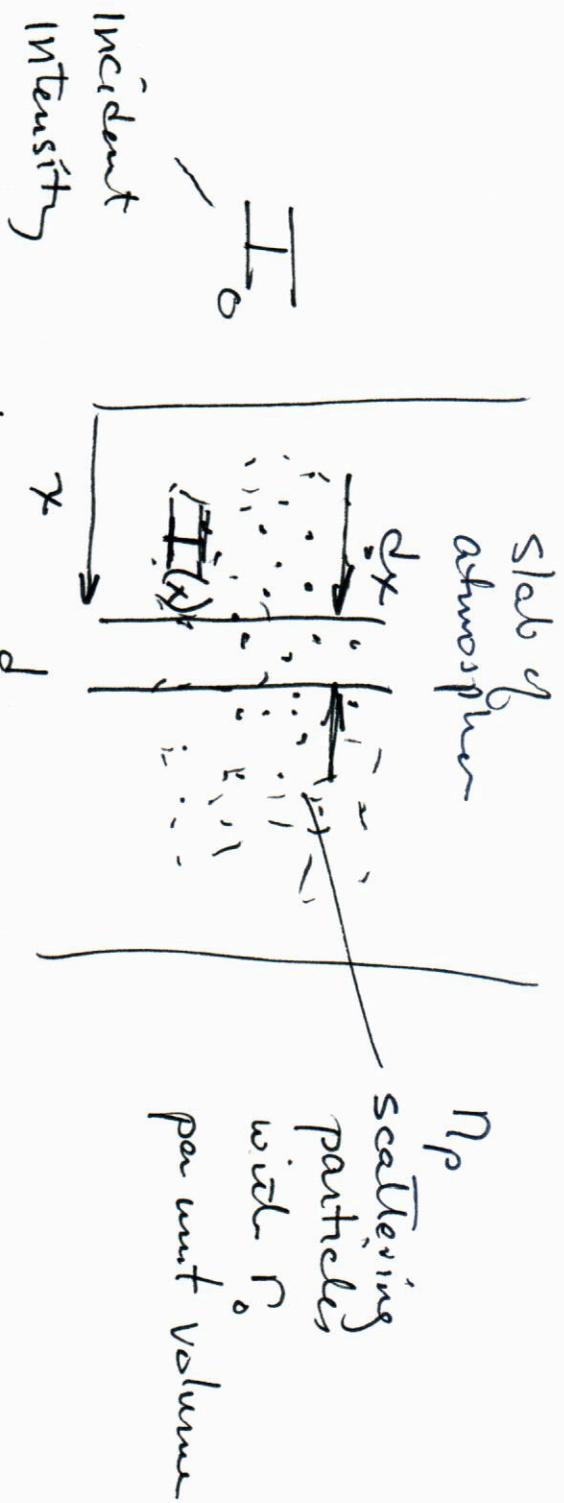
What determines  $S_{\theta}$ ? Radiation Scattering by air (small object), dust, aerosols, (RISER object)

Simple model of scattering:



ray strikes  
Suppose projected area of particle,  $A_{\text{part}} = \pi r_0^2$   
& there are  $N_p$  particles/volume.

Q: How does unscattered radiation behave with  $\Gamma_0$ ,  $N_p$ ?



$I(x) \sim$  unscattered intensity at position  $x$

$$dI(x) = -I(x) n_p dx$$

$$dI(x) = -\tau_{scatt} I(x) n_p dx$$

take  $\tau_{scatt} \approx \pi \Gamma_0^2$

$$\therefore I(x) = I_0 \exp(-x/l_{\text{scatt}})$$

where

$$l_{\text{scatt}} = (n_p \sigma_{\text{scatt}})^{-1} \\ = (n_p \pi r_0^2)^{-1}$$

$l_{\text{scatt}}$  is the mean-free path for light to travel in a dusty atmosphere

~~Some numbers:~~

~~$$r_0 \sim 10 \mu\text{m} = 10^{-5} \text{m}$$~~

~~$$n_p \sim 10 / \text{m}^3 \quad l_{\text{scatt}} \sim [10 \cdot 3 \cdot (10^{-5})^2]^{-1} = (3 \cdot 10^{-9})^{-1} \\ \approx 3 \times 10^{10} \text{m}!$$~~

~~$$100 / \text{m}^3 \quad \rightarrow l_{\text{scatt}} \sim 3 \times 10^7 \text{m} = 3 \times 10^4 \text{km}!$$~~

~~$$10^3 / \text{m}^3 \quad \rightarrow l_{\text{scatt}} \sim 3 \times 10^7 \text{m} = 3 \times 10^4 \text{km}!$$~~

Atmospheric Aerosol size & density can vary. Typ. Values:

$$r_0 \sim 1 \mu\text{m} \text{ or so}$$

$$M_p \sim 10^2 / \text{cm}^3 = 10^8 / \text{m}^3$$

$\therefore$

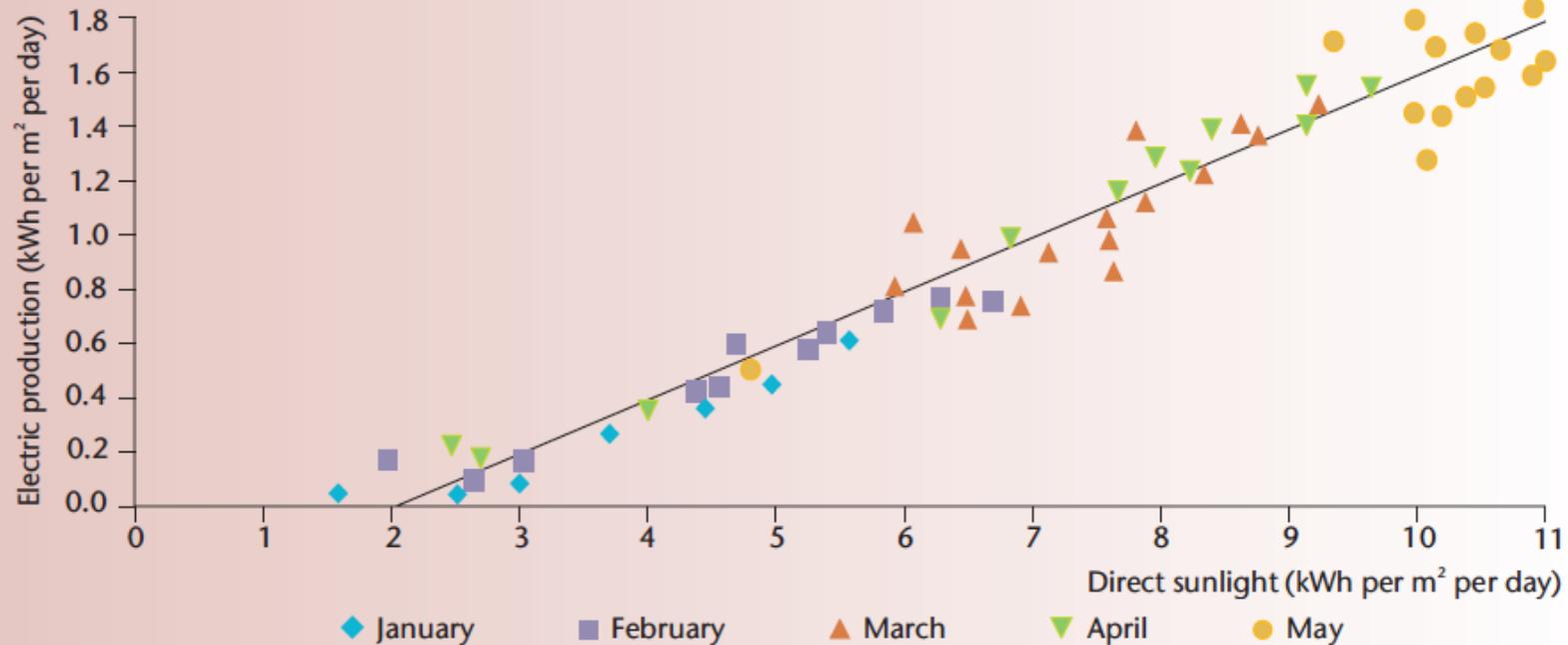
$$L_{\text{scatt}} \sim \frac{1}{n_p \pi r_0^2} \sim \frac{1}{10^8 \cdot 3 \cdot 10^{-12}} \sim \frac{10^4}{3} \sim \underline{\underline{300 \text{ m}}}$$

Implication: DNI will be reduced by scattering  
 DHI " " increased " "

$\text{DNI} \sim I_0 \exp(-\alpha' L_{\text{scatt}})$ ;  $\alpha'$  effective thickness of aerosol layer

# Require adequate DNI for CSP

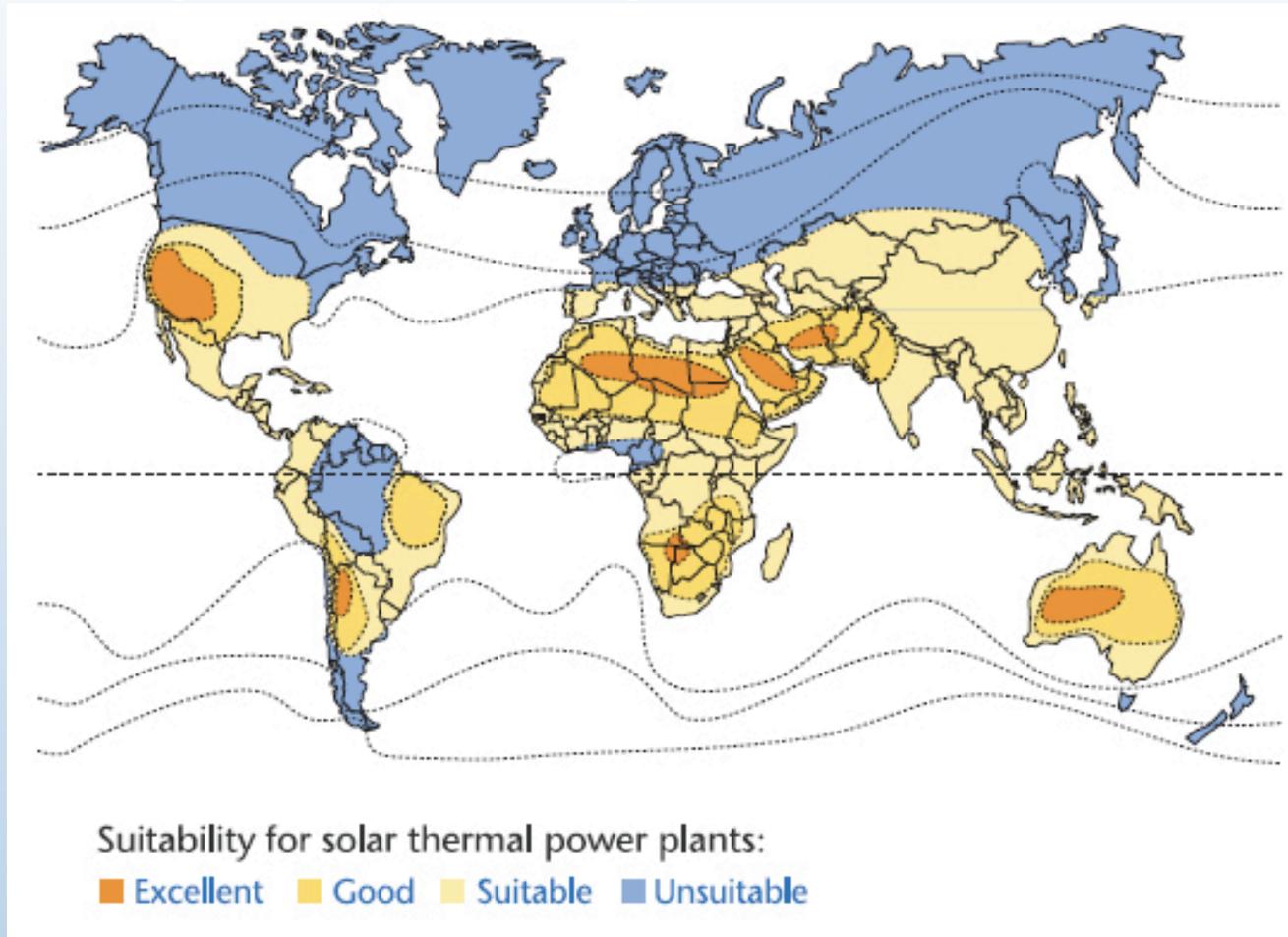
Figure 2: Output of an early CSP plant in California as a function of daily DNI



Source: Pharabod, F. and C. Philibert (1992), *Luz solar power plants*, DLR for IEA-SSPS.

# CSP Systems only use DNI

→ Only some regions are suitable



Q: Where are the good sites? Where are the demand centers?

# Sample Locations in the CONUS

## Merced, California

Latitude: 37.36

Longitude: -120.43

Altitude: 65m

## San Diego, California

Latitude: 32.88

Longitude: -117.23

Altitude: 104m

## Las Cruces, New Mexico

Latitude: 32.32

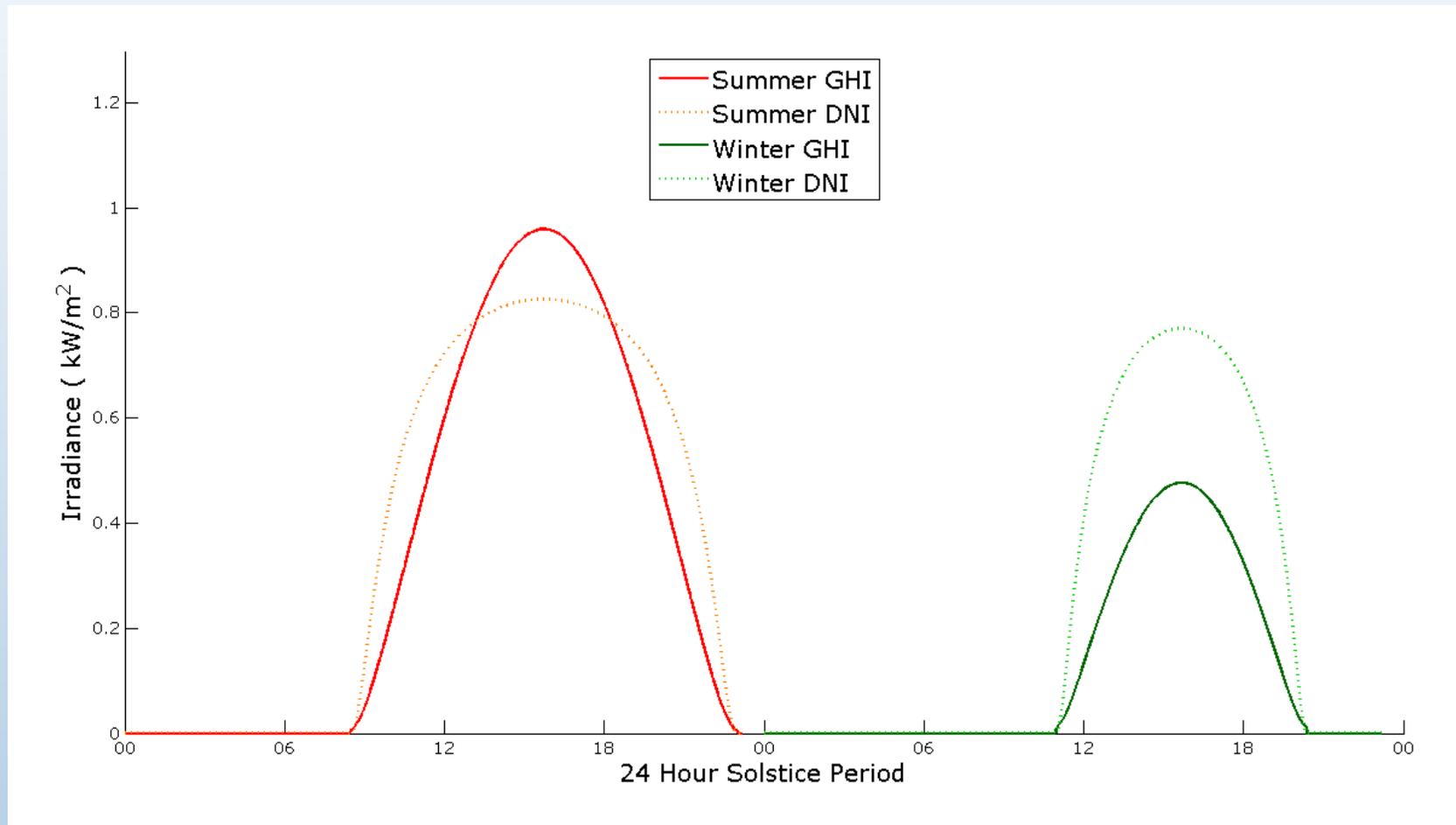
Longitude: -106.77

Altitude: 1219m



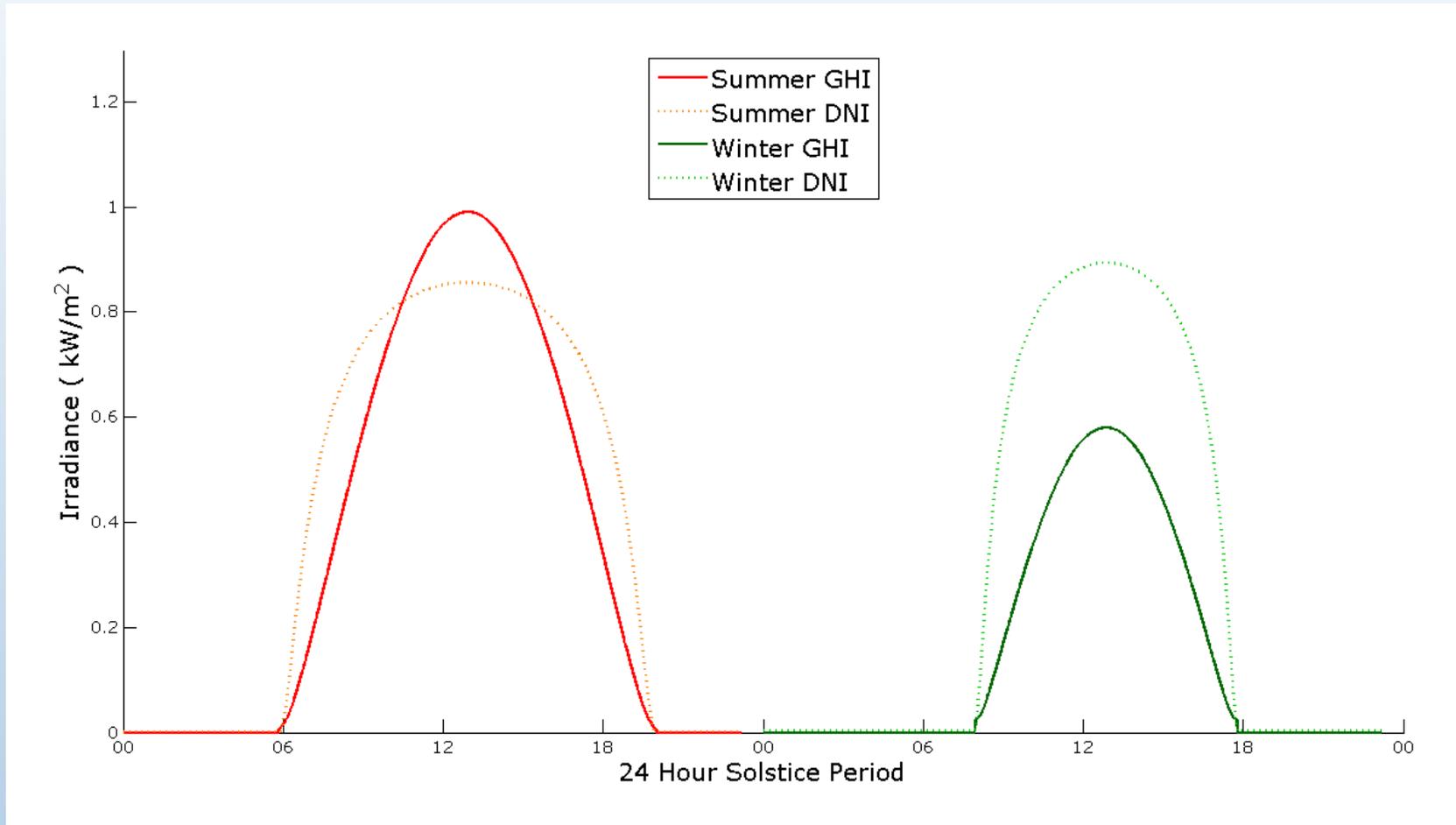
# Merced

Summer GHI Maximum	Winter GHI Maximum
0.8262	0.7702



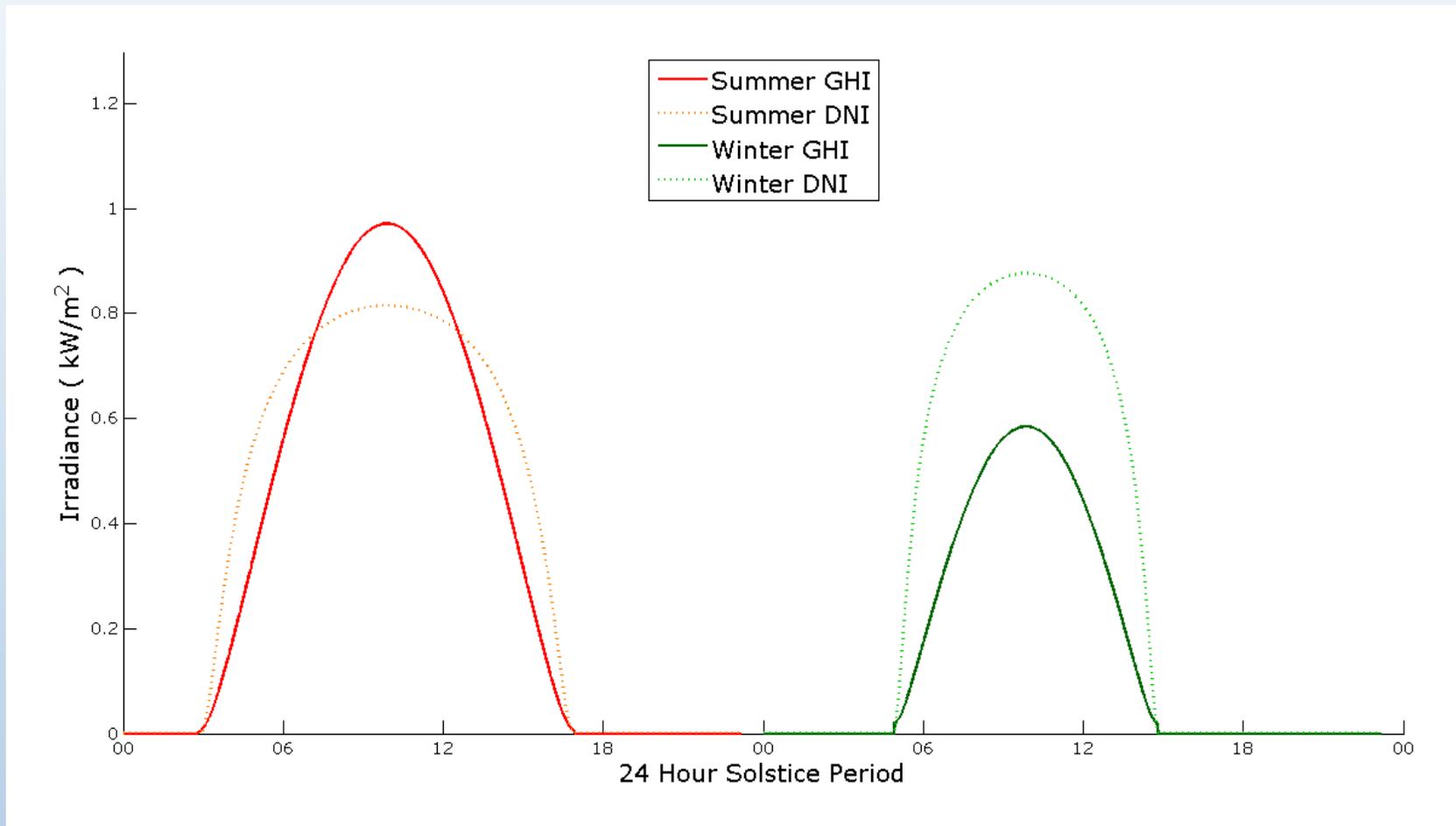
# San Diego

Summer GHI Maximum	Winter GHI Maximum
0.8560	0.8936



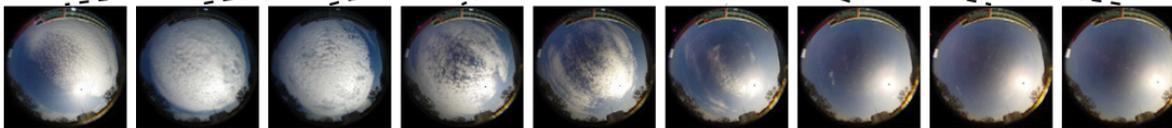
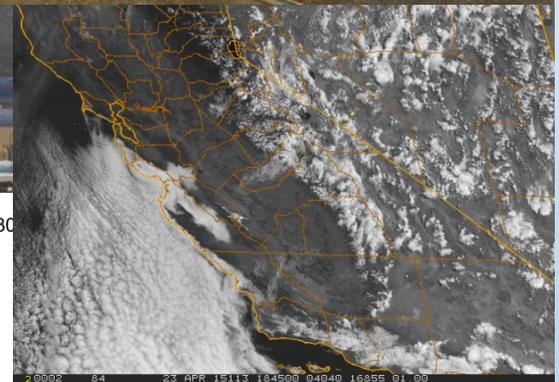
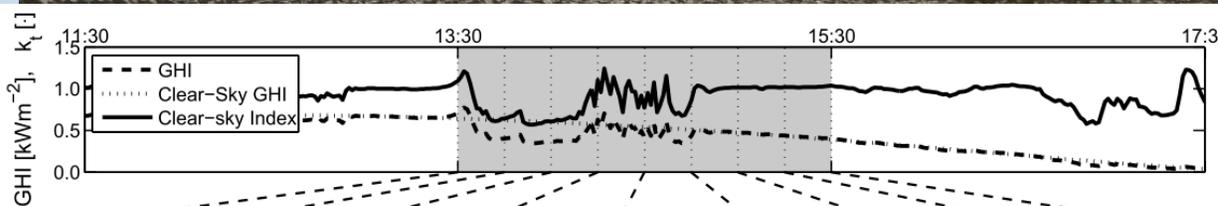
# Las Cruces

Summer GHI Maximum	Winter GHI Maximum
0.8153	0.8766



# Solar and Wind Forecasting for Large Power Plants

Prof. Carlos F. M. Coimbra UCSD MAE/CER





## Ivanpah Project Facts



### IVANPAH AT A GLANCE

The world's largest solar thermal project

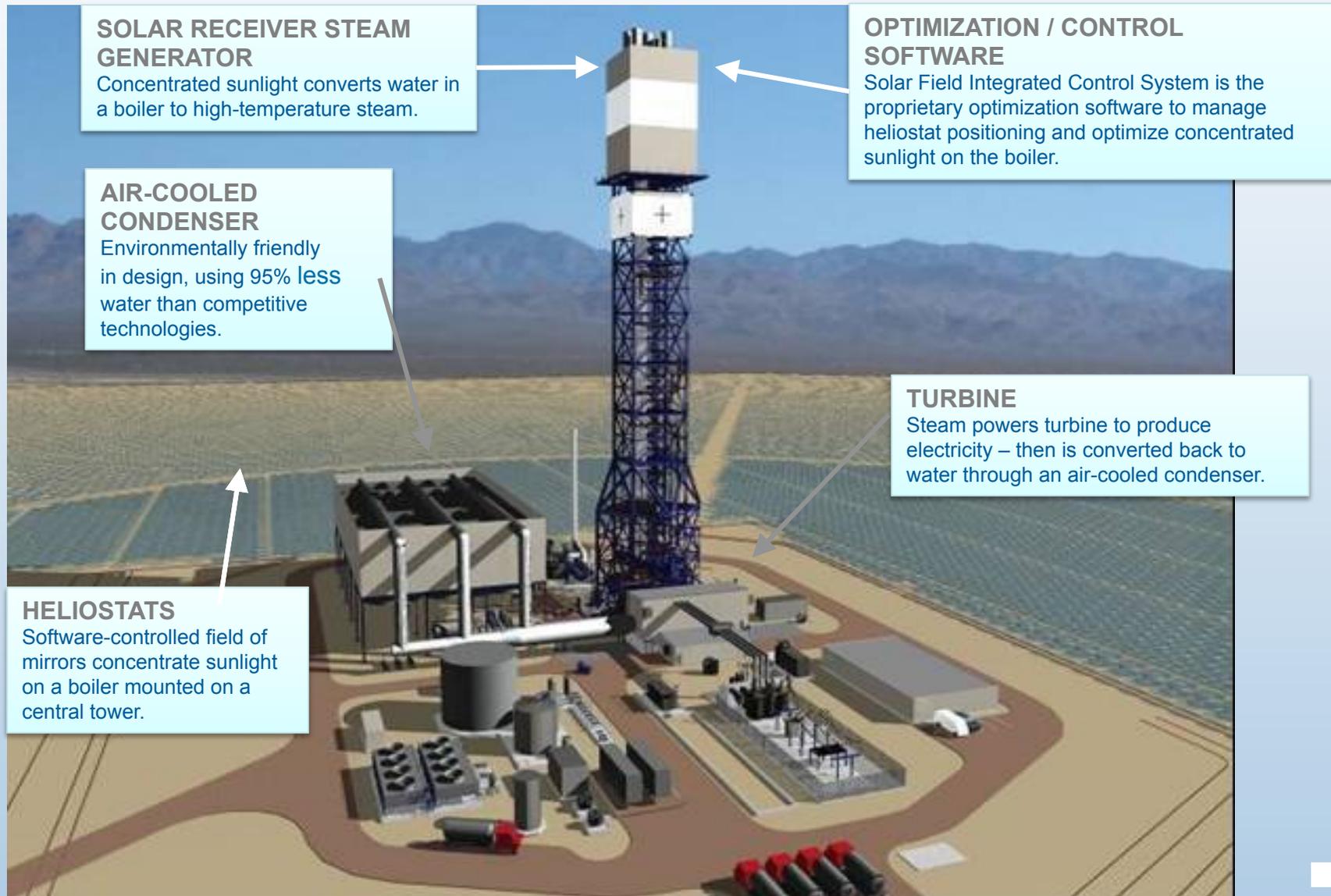
- Size: 3,600 acres
  - Power Production: 370 MW (nominal)
  - Homes Served Annually: 140,000
  - Customers: PG&E and SCE
  - Owners: NRG, Google, BrightSource
  - DOE Loan Guarantee: \$1.6B
  - Project Financing: \$2.2B
- 
- Construction Commenced: Oct 2010
  - Construction Status: **100%**
  - Construction workers: 2,000
  - Connected to Power Grid Since **2014**

# Utility Scale Central Plants

## Ivanpah Solar Energy Generation Systems, 392 MW

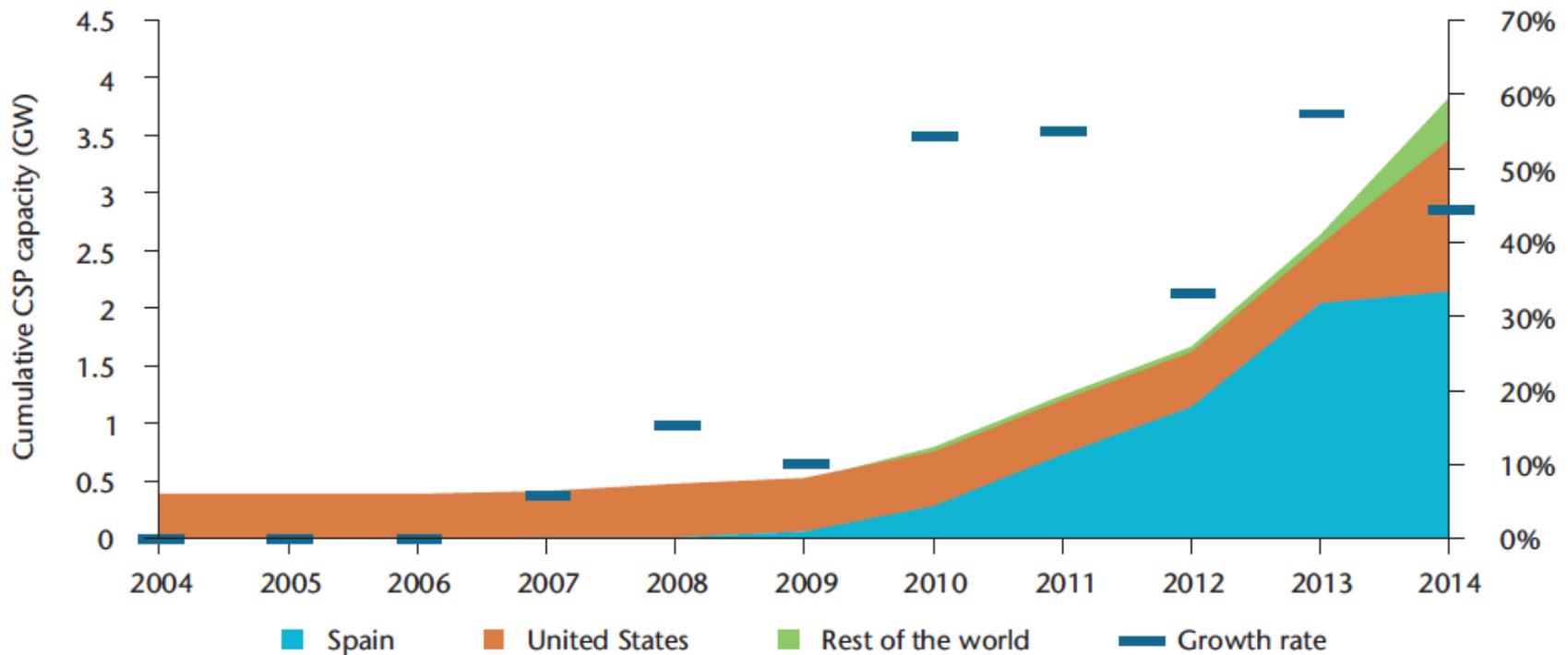


# Concentrated Solar Towers



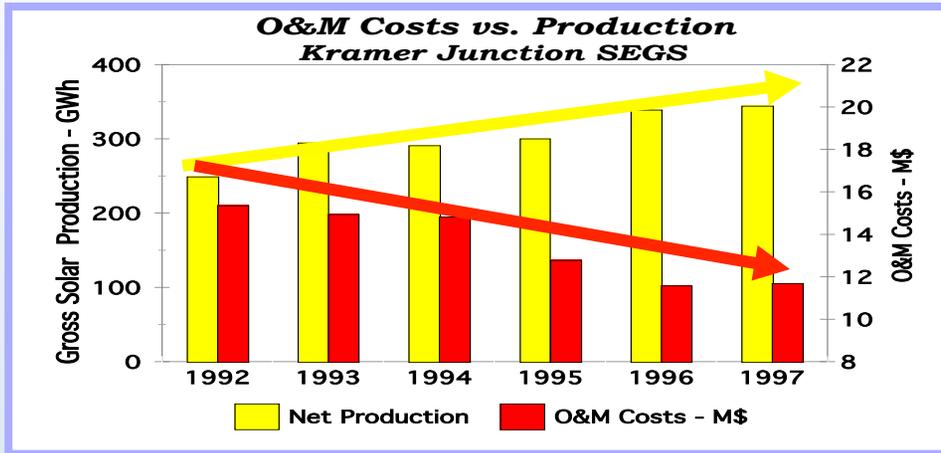
# Evolution of Installed Base - CSP

Figure 1: Global cumulative growth of STE capacity

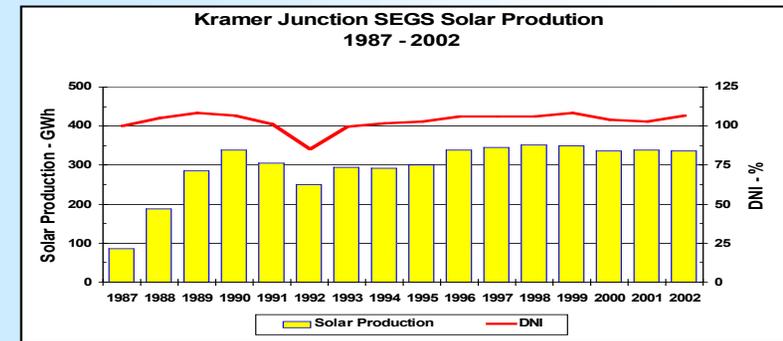


IEA, Solar Thermal Power Technology Roadmap, 2014

# SEGS Plant Experience (KJ)



## Kramer Junction Operational Experience Electrical Output

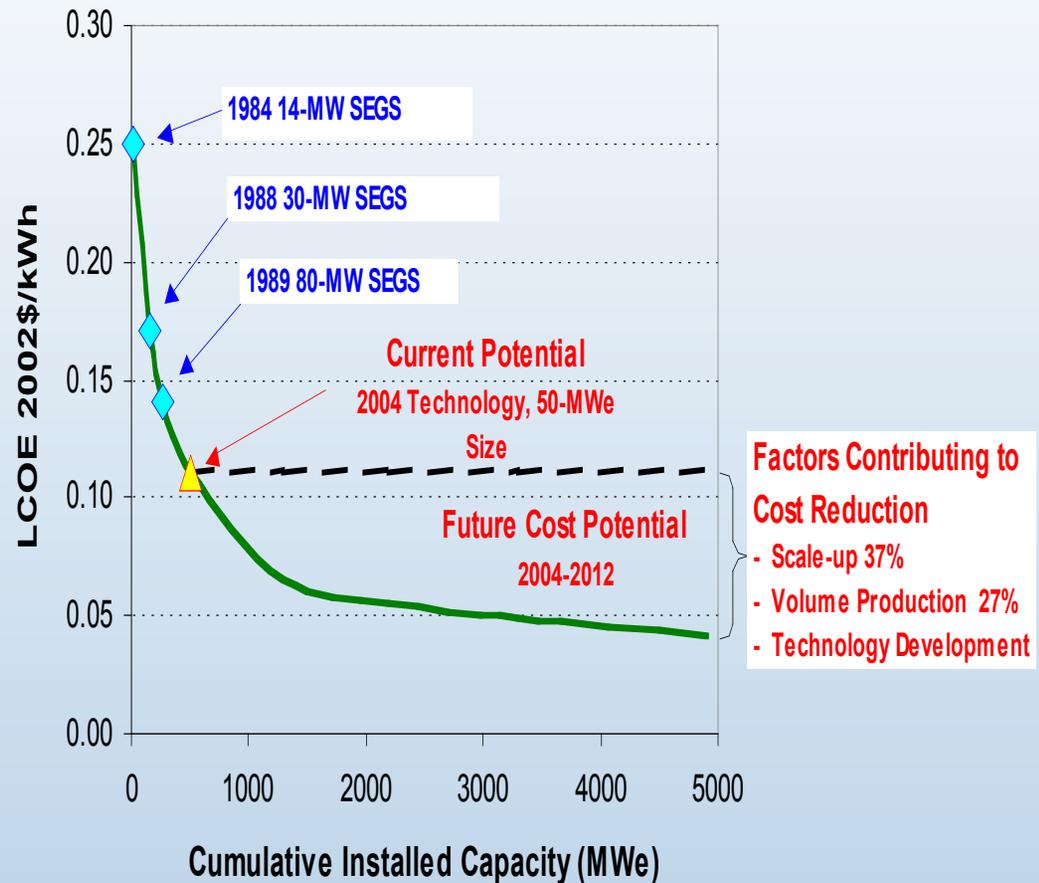


- O&M costs have dropped sharply over time, coincident with performance gains.
- These plants, placed in operation from 1987 through 1989, set many performance records in the 1990s.
- Using 25% energy input from natural gas via a supplemental boiler, capacity factors during SCE on-peak operation have exceeded 100% for more than a decade (with >85% from solar operation).

# Sargent & Lundy Cost Analysis

Cost reductions from

- Plant Scale Up
- Technology Development
- Volume Production



\* Sargent and Lundy (2003). Assessment of Parabolic Trough and Power Tower Solar Technology Cost and Performance Impacts. <http://www.nrel.gov/docs/fy04osti/34440.pdf>

# Solar Thermal Power System Plans

- Mojave Solar Park, USA California, 553MW, parabolic trough design[2]
- Pispah, USA California near Pispah north of I-40, 500MW, dish design[3]
- Ivanpah Solar, USA California, 400MW, power tower design[4]
- Unnamed, USA Florida, 300MW, Fresnel reflector design[5]
- Imperial Valley, USA California, 300MW, dish design[6]
- Solana, USA Arizona southwest of Phoenix, 280MW, parabolic trough design[7]
- Negev Desert, Israel, 250MW, design will be known after tender[8]
- Carrizo Energy Solar Farm, USA California near San Luis Obispo, 177MW, Fresnel reflector design[9]
- Uppington, South Africa, 100MW, power tower design[10]
- Shams, Abu Dhabi Madinat Zayad, 100MW, parabolic through design[11]
- Yazd Plant, Iran, 67MW steam input for hybrid gas plant, technology unknown.[12]
- Barstow, USA California, 59MW with heat storage and back-up, parabolic trough design[13]
- Victorville 2 Hybrid Power Project, 50MW steam input for hybrid gas plant, parabolic trough design[14]
- Kuraymat Plant, Egypt, 40MW steam input for a gas powered plant, parabolic trough design[15][16]
- Beni Mathar Plant, Morocco, 30MW steam input for a gas powered plant, technology unknown[17]
- Hassi R'mel, Algeria, 25MW steam input for gas powered plant, parabolic trough design[18]
- Cloncurry solar power station, Australia, 10MW with heat storage, power tower design[19]

Source: [http://en.wikipedia.org/wiki/List\\_of\\_solar\\_thermal\\_power\\_stations#Operational](http://en.wikipedia.org/wiki/List_of_solar_thermal_power_stations#Operational)

# Solar Thermal Power Technology

## Achievements and Status

- 350 MW of parabolic trough plants built around 1990 still operating well
- Several power tower demonstration plants have established technology viability.
- Several dish systems have also operated successfully
- Engineering cost analyses indicate 5 cents/kWh achievable

## Likely Advances

- There are major opportunities for technology advances, in
  - Collectors
  - Power conversion
  - Thermal storage
- Several new systems will be built within 5 years
- Their success should catalyze manufacturing advances, commercialization